

## ARTICLE

**Gamma-ray Imaging System with a Rotation Collimator**

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The performance of a gamma-ray imaging system consisting of a gridded collimator and coaxial NaI(Tl) detector was investigated. A gamma-ray imaging system with rotation collimators does not require a position-sensitive detector so as to find the location of gamma-ray sources and therefore this feature allows for significant amount of flexibility not only detector selection but also the geometry of the system. A reconstructed image from the  $^{137}\text{Cs}$  gamma-ray source have been obtained by using the simple flat-fielded back-projection algorithm. The background events are jumbled together in the correct modulation-patterns. Therefore a possibility may be caused by those events that the image is reconstructed at random on the image plane. The theoretical image resolution for the current proof-of-principle gamma-ray imager is  $\sim 1^\circ$  with a FOV  $\sim 53.6^\circ$ . The image resolution with FWHM shows about  $11.2^\circ$ . Therefore our gamma-ray imaging system is required the more collimators, because the reconstructed image was significantly affected by the modulation patterns. Future research will be to focus on the improvement of the image resolution with two or more collimators.

**KEYWORDS:** modulation pattern, image reconstruction, NaI(Tl) detector, gridded collimator

**I. Introduction**

Rotating modulation collimators (RMCs) are one of the techniques for gamma-ray imaging using a mechanical collimator. Unlike pin-hole collimator or coded aperture, RMCs make with a single-channel detector to record a time-dependent modulation-pattern that involves a location information of interest gamma-ray sources. A basic RMC consists of a detector located beneath a gridded collimator. Currently, the RMC method is using to get a reconstructed image of the sun in the Reuven Ramaty High Energy Solar Spectroscopic Imager (RHESSI) and the RHESSI allowed for excellent performance of the infinite focus of solar imaging. The gamma-ray imaging system using RMCs has been studied for astronomical, medical application, and homeland security.<sup>1-4)</sup>

The greatest advantage of the RMC imager is that this system does not requires a position-sensitive detector so as to find the location of the gamma-ray source and their ability to achieve good image resolution over a relatively wide field-of-view (FOV).<sup>3)</sup> Therefore this feature allows for significant amount of flexibility not only detector selection but also the geometry of the system. And this system is a non-spectroscopic system, the data acquisition systems can be made relatively simple depending on the objective.

Many assumptions that are valid for a focus of infinity such as RHESSI are no longer valid in the near-field environment so that the incident gamma-ray as not parallel.<sup>4)</sup> To that reason, we have designed and tested the proof-of-principle system for the gamma-ray as well as neutron imaging in the future.

**II. Principle of Image Reconstruction**

The rotating collimator temporally modulates the intensity of the gamma-ray flux transmitted to a detector. Thus the rotation causes the transmission of the grid viewing a gamma-ray

source that was a modulated count-rates; the modulation pattern depends on the location of the source in the FOV. The image resolution ( $\Delta\theta$ ) and FOV for the gamma-ray imaging system are defined as<sup>3)</sup>:

$$\begin{aligned}\Delta\theta &= \tan^{-1}\left(\frac{0.5p}{D_d}\right) \\ \text{FOV} &= \frac{R_c + R_d}{D_d}\end{aligned}\quad (1)$$

where  $p$  is the width of grid-pitch,  $D_d$  is the distance between collimator and detector, and,  $R_c$  and  $R_d$  is the radius of detector and collimator, respectively.

Because the measured data is only an indirect measurement of the image, a suitable treatment of the modulated count-rates produces an image in gamma-rays. The ideal modulation function  $I_m(\theta)$  means the probability of detecting counts from a point source located at position  $m$ , when the collimator is at angle  $\theta$ <sup>5,6)</sup>:

$$I_m = \frac{I_0\varepsilon}{2} \left| 1 - \frac{r_m \cos(\theta - \theta_m)}{\Delta} + \text{Int} \left[ \frac{r_m \cos(\theta - \theta_m)}{\Delta} \right] \right| \quad (2)$$

where  $\varepsilon$  is the detection efficiency,  $\text{Int}[x]$  is the integer which satisfies  $\text{Int}[x] \leq x < \text{Int}[x+1]$  and  $0 \leq \theta < \pi$ ,  $I_0$  is the incident flux of the gamma-ray source in  $\text{counts}/\text{cm}^2/\text{sec}$ , and  $\Delta$  is grid pitch of the collimator.

For image reconstruction, we are currently employing an intermediate image which is called the simple flat-fielded back-projection algorithm. The modulation patterns  $I_m(\omega t)$  are calculated and then added on the image voxel  $m$  every time  $t$  with angular velocity  $\omega$  of the collimator. The simple flat-fielded back-projection algorithm has been of the form<sup>7)</sup>:

$$S_m = \frac{\sum_t O(t)(I_m(\omega t) \langle I_m \rangle)}{AT(\langle I_m^2 \rangle \langle I_m \rangle^2)} \quad (3)$$

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where  $S_m$  is the estimated probability that location of gamma-ray source is the  $m$ th voxel,  $O(t)$  represents the observed counts at time  $t$ ,  $A$  is the effective area of the detector, and,  $T$  is the total livetime in seconds.

Therefore, reconstruction of images required a knowledge of  $I_m(\omega t)$  for the gridded collimators as a function energy and direction of the incidence since the image sensitivity is proportional to the variance of the ideal modulation function for each image voxel.

### III. Gamma-ray Imaging System

**Figure 1** shows a photograph of the our gamma-ray imaging system. Gamma-ray imaging system consisting of a gridded collimator and coaxial NaI(Tl) detector manufactured by Bicron. The purpose of the data acquisition system is to record the time and number of each gamma-ray detected, allowing the modulated count-rates to be determined as a function of rotation angle. Since RMC imaging system does not requires a position-sensitive detector, the NaI(Tl) detector have a suitable capabilities for the proof-of-principle system.



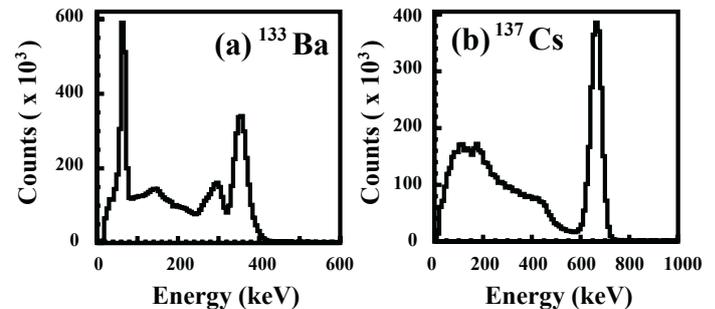
**Fig. 1** Photograph of our Gamma-ray imaging system.

The NaI(Tl) crystal diameter and thickness are 76.2 mm, equally. And the applied high-voltage was +800 V. The tungsten collimator has a diameter of 90.0 mm and 2.0-mm-thick. The grid pitch and slit are 2 mm and 1 mm in width, respectively. The gridded collimator is mounted on the gear. The distance between collimator and detector is 55 mm, and the angular velocity  $\omega$  is setting up about 0.25 revolutions per minute by using stepping-motor control system. Hence, theoretical image resolution for the current proof-of-principle gamma-ray imager is  $\sim 1^\circ$  with a FOV  $\sim 53.6^\circ$ .

### IV. Experimental Results

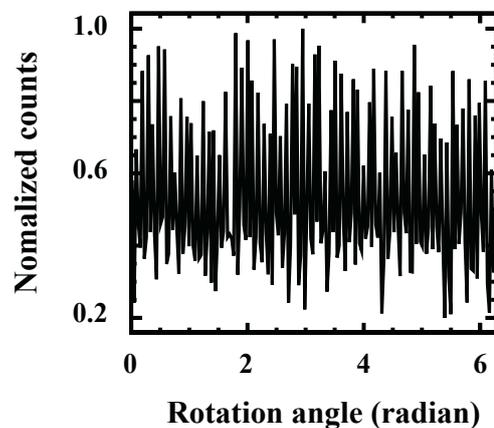
**Figure 2** shows gamma-ray energy spectra of the NaI(Tl) detector for the standard gamma-ray source  $^{133}\text{Ba}$  and  $^{137}\text{Cs}$ . A NaI(Tl) detector output was fed into a scintillation preamplifier (ORTEC-113) and then into a spectroscopy amplifier (ORTEC-672). The output of spectroscopy amplifier was read on a multichannel buffer (ORTEC-919) for the energy measurement. A background noise due to the stepping-motor control system of the collimator was picked up the pho-

tomultiplier tube (PMT) base of the NaI(Tl) detector. Therefore, PMT base were enclosed in aluminum foil to protect against noise from the stepping-motor control system. The energy resolution was about 61.2 keV in full width at half maximum (FWHM) at 661.6 keV after channel calibration of multichannel buffer with gamma-ray peaks in a  $^{133}\text{Ba}$  (81.0 keV),  $^{137}\text{Cs}$  (661.6 keV), and,  $^{60}\text{Co}$  (1173.2 keV and 1332.5 keV) source.



**Fig. 2** Gamma-ray energy spectra with the present Gamma-ray imaging system for two gamma-ray sources, (a)  $^{133}\text{Ba}$  and (b)  $^{137}\text{Cs}$ .

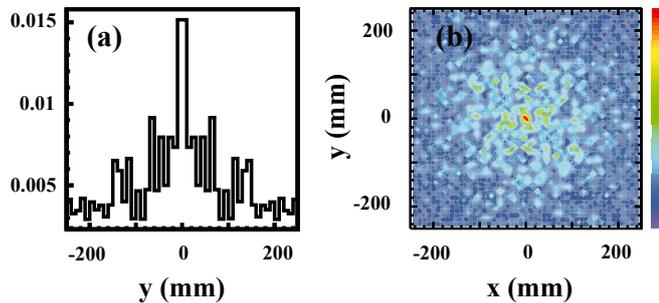
The experimental data for the image reconstruction recorded the counting numbers at one-second interval by using ORTEC-850 Quad Single-Channel Analyzer (SCA) and ULS-3000 4-Channel Counter/Timer/Rate Meter. The data acquisition software is a program offered by ULS Inc. and it is implemented and operated on a PC Window system.



**Fig. 3** Modulation patterns obtained by the our gamma-ray imaging system with the  $^{137}\text{Cs}$  gamma-ray source.

A  $10 \mu\text{Ci}$   $^{137}\text{Cs}$  source were 100 mm from the gridded collimator and **Figure 3** shows an experimental modulation pattern. However, because of the close proximity of the gamma-ray source or single collimator, there are such background events as the gamma-rays pass through without interaction with collimator or a grid space of collimator. Those events are jumbled together in the correct modulation-patterns. Therefore a possibility may be caused by those events that the image is reconstructed at random on the image plane. However, if the sum of the modulation patterns and background is sim-

ilar to the  $I_m(\omega t)$  at  $r_m \sim 0$ , such events are reconstructed on the central region of image plane.



**Fig. 4** The profile and two-dimensional image for a  $^{137}\text{Cs}$  source obtained from the experimental data.

**Figure 4** shows a profile and reconstructed image for gamma-ray source  $^{137}\text{Cs}$ . The image plane is perpendicular to the  $z$ -axis and 155.0 mm from the face of the detector and the size of image voxel is 10.0 mm x 10.0 mm. The  $S_m$  in the Eq. (3) is calculated for each image voxel as the location of real gamma-ray source by using the ROOT software library.<sup>8)</sup> Due to the geometry of the gridded collimator, the reconstructed image will not stand for a location of gamma-ray at the central extent around the image resolution in the Eq. (1) as well as the outside FOV of the gamma-ray imaging system. In order to evaluate the image resolution of the gamma-ray imaging system, the one-dimensional profile were selected in a  $\pm 10$  mm on the  $x$ -axis. The image resolution with FWHM shows about  $11.2^\circ$ . The reconstructed image is more blurred than the expected image resolution and the random images are reconstructed on the image plane because of the background events.

Consequently, the image reconstruction was significantly affected by the modulation patterns, this proof-of-principle system shows not enough to obtain an accurate location of the gamma-ray source with single collimator. Future research will be focus on the improvement of the image resolution with the two or more collimators.

## V. Summary

The performance of a gamma-ray imaging system consisting of a gridded collimator and coaxial NaI(Tl) detector was investigated. A gamma-ray imaging system with rotation collimators does not require a position-sensitive detector so as to find the location of gamma-ray sources and therefore this feature allows for significant amount of flexibility not only detector selection but also the geometry of the system. A reconstructed image from the  $^{137}\text{Cs}$  gamma-ray source have been obtained by using the simple flat-fielded back projection algorithm. The background events are jumbled together in the correct modulation-patterns. Therefore a possibility may be caused by those events that the image is reconstructed at random on the image plane. The theoretical image resolution for the current proof-of-principle gamma-ray imager is  $\sim 1^\circ$  with a FOV  $\sim 53.6^\circ$ . The image resolution with FWHM shows about  $11.2^\circ$ . Therefore our gamma-ray imaging system is required the more collimators, because the reconstructed image was significantly affected by the modulation patterns. Future research will be to focus on the improvement of the image resolution with two or more collimators.

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