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ARTICLE

Radiation impact of very low level radioactive steel reused in motorway tunnel constructions

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Considerable amount of radioactive materials arising from decommissioning of nuclear power plants may be classified as very low level radioactive waste. Various types of mentioned radioactive materials were analyzed in several international documents devoted to the optimization of radioactive material management with emphasis on concepts of recycling and reuse. One of these concepts of optimization is the conditional clearance of materials with their subsequent recycling and reuse in industrial sector. The concept of conditional clearance of radioactive materials into the environment follows international recommendations derived from the principles that the individual effective dose received by critical individual must not exceed some tens of μ Sv/yr. This paper deals with the radiation impact of recycling and reuse of conditionally cleared steel in industrial sector, specifically in motorway tunnel constructions. Scenario of the reuse of radioactive steel in form of reinforcing mesh and bars was created based on the data acquired from current motorway building practice in the Slovak Republic. The aim of the paper is to assess the radiation impact and to justify new specific clearance levels for radionuclides contained in steel reinforcement components in order to clear and reuse maximum amount of very low level radioactive steel considering mentioned dose criterion.

Keywords: conditional clearance; decommissioning; dose rates; exposure pathways; clearance levels; VISIPLAN 3D ALARA; GOLDSIM

1. Introduction

Nowadays, management of radioactive waste represents a world-wide discussed topic. There exist international incentives to minimize amount of radioactive waste using various concepts of clearance. Dose criteria applied for the clearance of radioactive materials was determined in order to ensure the protection to the public from radiation exposure. Conditional clearance represents alternative approach that also meets these health protection limits. In general, this alternative approach may lead to higher clearance limits compared to unconditional clearance while the protection of public is being achieved at the same level [1]. The concept of conditional clearance includes following requirements:

- Mainly solid metal radioactive materials are taken into account.
- Materials contain mostly relatively short-lived radionuclides.
- Long-term fixing of short-lived radionuclides in specific, previously defined, industrial constructions is required (this ensures significant reduction of radioactivity and possible detrimental impacts).
- Dose criteria (DC) of individual effective dose of

some tens of μ Sv/year and collective effective dose of 1 man Sv/year based on international recommendation [2,3].

However, current legislation of the Slovak Republic (Statutory Order No. 345/2006 Coll.) stipulates the constraint of individual effective dose as 10 μ Sv/year or 50 μ Sv/year considering specific conditions.

2. Motorway tunnel scenario

2.1. Basic information

Motorway tunnel scenario is based on the data on real tunnel construction comprising two tunnel tubes, which will carry the unidirectional traffic during a standard operation. The total lengths of the modeled tunnel tubes are 2 km. This length is chosen because it represents approximately the average length of existing tunnel constructions in the Slovak Republic. The reinforcement of the tunnel consists of primary and secondary lining. Following two possibilities were indentified based on specific analysis of optimal reuse of reinforcing components made from very low level (VLL) radioactive steel:

- Bars bound together in reinforcement cage of the strip foundation in secondary lining.
- Two layers of steel reinforcing mesh in primary lining.

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Melting and Reinforcing Components Production	W – Worker	M – Member of the Public	Long-term Period
Inhalation – W	Motorway Tunnel Building Stage	Motorway Tunnel Operation Stage	Inhalation – M
Ingestion – W Skin Contamination – W	No internal exposure is assumed	No internal exposure is assumed	Ingestion – M Skin Contamination – M
External Exposure – W	External Exposure – W	External Exposure – W, M	External Exposure – M
$T_0 = 0$ years	3 years	100 years	10 000 years

Figure 1. Scheme of exposure pathways relevant for motorway tunnel scenario

2.2. Methodology

The impact assessment methodology of the reuse of very low level radioactive steel in form of reinforcement mesh and bars, which partially arises out of the international methodology for the application of the concepts of exclusion, exemption and clearance [2,3] comprises following steps:

- 1. Determination of nuclide vector composition contained in conditionally cleared metals.
- 2. Definition of set of tunnel construction parameters and related performed activities.
- 3. Development of geometrical, radiological and material model of selected enveloping scenarios.
- 4. Calculation of received annual individual effective doses for each relevant exposure pathway.
- 5. Identification of the critical individual in limiting enveloping scenario for each set of calculations.
- 6. Derivation of new clearance levels for limiting scenario for each considered radionuclide.

The last step of analysis is represented by calculation of amount of radioactive metal materials arising from decommissioning of given NPP that can be conditionally cleared and reused safely in motorway tunnel.

2.3. Relevant exposure pathways

Radiological impact analysis was divided into following four stages (four timescales were considered):

- Melting of metal radioactive material and production of reinforcing components in controlled area (3 years).
- Building of motorway tunnel (3 years).
- Operation of motorway tunnel (100 years).
- Long-term radiological impacts (10 000 years).

Exposure pathways (EP) such as inhalation, ingestion and skin contamination are considered in case of radionuclides occurrence in dust, water or food causing possible intake of these radionuclides by workers or members of the public. Radionuclides may be generated in the form of dust or aerosols also during some specific thermal processes such as melting, welding or using cutting torch. Based on the data from current industrial practice, no thermal processes are used during building of motorway tunnel and operational stage, therefore no internal exposure is assumed due to negligible level of dust/aerosols generation.

Relevant exposure pathways identified for the motorway tunnel scenario are depicted on **Figure 1**. In general, four exposure pathways were indentified: external exposure (EXT), inhalation (INH), ingestion (ING) and skin contamination (SKIN).

2.4. Radiological impact assessment

2.4.1 Analyzed nuclide vector

Table 1 includes selected radionuclides analyzed indose assessment based on radiological characterizationof A1 NPP located in the Slovak Republic.

Table 1. List of radionuclides considered in assessment

Exposure pathway	Considered radionuclides	
External Exposure (EXT)	⁶⁰ Co, ⁹⁴ Nb, ¹²⁶ Sn, ¹³⁷ Cs, ¹⁵² Eu, ²³⁹ Pu	
Inhalation (INH) Ingestion (ING) Skin Contamination (SKIN)	³ H, ⁵⁹ Ni, ⁶⁰ Co, ⁶³ Ni, ⁹⁰ Sr, ⁹³ Mo, ⁹³ Zr, ⁹⁴ Nb, ⁹⁹ Tc, ¹²⁶ Sn, ¹²⁹ I, ¹³⁷ Cs, ¹⁵¹ Sm, ¹⁵² Eu, ²³⁸ Pu, ²³⁹ Pu, ²⁴¹ Am	

Sets of radionuclides considered in particular exposure pathways differ due to natural behavior of particular radionuclides (i.e. only gamma radiation emitters are considered in external exposure pathway).

2.4.2 Results

Assessment of possible exposure pathways relevant for melting, construction, operation and long-term period was performed. Internal exposure and skin contamination of workers conducting activities related to the melting stage was performed based on equations, parameters and approaches applied in international recommendations [3]. The computational tool VISIPLAN 3D ALARA was used for calculation of external individual effective doses [4]. The simulation software GOLDSIM was used for the assessment of long-term impacts. GOLDSIM environment enables modeling of degradation processes and transport of radionuclides through unsaturated and saturated zone of subsoil [5].

Stage	Performed activity / enveloping scenario	Annual exposure time (hours)	Annual received individual effective dose (µSv)	Specific mass activity contained in metal material (Bq/kg)
	Cutting and manipulation	1 100	33.17	301.5
Melting and	Melting and slag handling	715	4.91	301.5
Reinforcing	Storage of ingots/reinforcing components	220	5.02	300
Components	Manufacture of reinforcing components	770	1.28	300
Production Stage	Manipulation of manufactured re-bars	660	3.74	300
	Transport of reinforcing components	150	1.50	300
	Assembly of primary lining (PL)	1 925	6.17	300
Building Stage	Assembly of strip foundation	550	2.55	300
	Realization of secondary lining	840	2.31	300
	Storage of steel mesh and re-bars	58	2.39	300
Operation Stage	Maintenance of already built tunnel	130	9.53E-03	300
	Professional driver	50	5.20E-03	300
	Driver or passenger	10	1.04E-03	300
Long-term Period	Inhabitant with garden	8760 (whole year)	1.13E-08	300

Table 2. Results of radiation impact assessment for radionuclide ⁶⁰Co

Parameters related to impact assessment were acquired from tunnel construction experts, international documents published by IAEA or European Commission [3,6] and reports dealing with dose assessment of workers during melting process.

Radiation impact assessment of last 3 stages considers specific mass activity 300 Bq/kg contained in material.

In case of melting stage, it is necessary to bear in mind distribution of radioactivity during melting process [7]. Therefore specific mass activity of metal components before melting was recalculated using distribution coefficients. Furthermore, it is assumed that melting and reinforcing components production would take a place in controlled area. Therefore dose limit of 20 mSv/year is relevant for this stage.

 Table 2 contains example of calculated individual

 effective doses received by workers or members of

 public performing analyzed activities.

The same calculations were performed for each analyzed radionuclide. Aim of the assessment is to identify critical individual or limiting enveloping scenario (ES) respectively.

2.5. Clearance levels

The derivation of the new clearance levels (CL) is performed by following formula ensuring that radiation protection criteria will be met:

$$A = \frac{D_C}{IED} A_u \tag{1}$$

Where:

- A Specific activity concentration of radionuclide (clearance level),
- D_{C} Dose criterion (10 µSv/year or 50 µSv/year),
- IED Calculated annual individual effective dose received by individual in limiting scenario,

A_u – Reference value of specific mass activity.

Derived values of new clearance levels can be seen in **Table 3** and **Table 4** along with limiting enveloping scenario and exposure pathway. Tables also include limit value of specific mass activity for unconditional clearance (UC) defined in Slovak legislation.

Derived clearance levels of few radionuclides (¹²⁹I and ⁹³Zr) are even lower than UC limit values. This fact can be caused by undue level of conservatism applied in assessment of melting stage, which could lead to overestimating of received doses. Furthermore no measures for restriction of internal exposure during melting stage were considered.

Table 3. Derived CL considering 10 µSv/year dose criterion

Nuclide	UC limit value (Bq/kg)	Derived CL (Bq/kg)	Limiting ES	Limiting EP
³ H	3,00E+06	1,80E+09	Melting	ING
⁵⁹ Ni	3,00E+05	1,10E+08	Inhabitant	ING
⁶⁰ Co	3,00E+02	4,80E+02	Assembly of PL	EXT
⁶³ Ni	3,00E+06	2,90E+08	Inhabitant	ING
⁹⁰ Sr	3,00E+03	1,40E+05	Cutting and Manipulation	SKIN
⁹³ Mo	3,00E+04	6,90E+06	Inhabitant	ING
⁹³ Zr	3,00E+05	6,00E+04	Melting	INH
⁹⁴ Nb	3,00E+02	6,50E+02	Assembly of PL	EXT
⁹⁹ Tc	3,00E+05	1,90E+07	Inhabitant	ING
¹²⁶ Sn	3,00E+03	2,10E+04	Assembly of PL	EXT
¹²⁹ I	3,00E+04	1,10E+04	Melting	ING
¹³⁷ Cs	3,00E+02	1,80E+03	Assembly of PL	EXT
¹⁵¹ Sm	3,00E+05	1,10E+07	Melting	INH
¹⁵² Eu	3,00E+02	9,80E+02	Assembly of PL	EXT
²³⁸ Pu	3,00E+02	3,90E+03	Melting	INH
²³⁹ Pu	3,00E+02	9,80E+02	Melting	INH
²⁴¹ Am	3,00E+02	1,20E+03	Melting	INH

Table 4. Derived CL considering 50 μ Sv/year dose criterion

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Nuclide	UC limit	Derived CL	Limiting ES	Limiting
		value (Bq/kg)	(Bq/kg)	Limiting ES	EP
		3,00E+06	1,80E+09	Melting	ING
		3,00E+05	5,50E+08	Inhabitant	ING
		3,00E+02	2,40E+03	Assembly of PL	EXT
93 Mo 3,00E+03 1,44E+05 Manipulation SKIN 93 Mo 3,00E+04 3,50E+07 Inhabitant ING 93 Zr 3,00E+05 6,00E+04 Melting INH 94 Nb 3,00E+02 7,70E+02 Cutting and Manipulation EXT 99 Tc 3,00E+05 9,80E+07 Inhabitant ING 126 Sn 3,00E+03 1,10E+05 Assembly of PL EXT 129 I 3,00E+04 1,08E+04 Melting ING 127 Ss 3,00E+02 2,10E+03 Cutting and Manipulation EXT 137 Cs 3,00E+05 1,08E+07 Melting INH 151 Sm 3,00E+05 1,20E+03 Cutting and Manipulation EXT 152 Eu 3,00E+02 1,20E+03 Cutting and Manipulation EXT 238 Pu 3,00E+02 3,88E+03 Melting INH 239 Pu 3,00E+02 9,80E+02 Melting INH	⁶³ Ni	3,00E+06	1,50E+09	Inhabitant	ING
		3,00E+03	1,44E+05	U	SKIN
94 Nb $3,00E+02$ $7,70E+02$ Cutting and Manipulation EXT 99 Tc $3,00E+05$ $9,80E+07$ Inhabitant ING 126 Sn $3,00E+03$ $1,10E+05$ Assembly of PL EXT 129 I $3,00E+03$ $1,10E+05$ Assembly of PL EXT 129 I $3,00E+04$ $1,08E+04$ Melting ING 137 Cs $3,00E+02$ $2,10E+03$ Cutting and Manipulation EXT 151 Sm $3,00E+05$ $1,08E+07$ Melting INH 152 Eu $3,00E+02$ $1,20E+03$ Cutting and Manipulation EXT 238 Pu $3,00E+02$ $3,88E+03$ Melting INH 239 Pu $3,00E+02$ $9,80E+02$ Melting INH		3,00E+04	3,50E+07	Inhabitant	ING
99 Tc $^{3,00E+02}$ $^{7,70E+02}$ Manipulation EX1 99 Tc $^{3,00E+05}$ $^{9,80E+07}$ Inhabitant ING 126 Sn $^{3,00E+03}$ $^{1,10E+05}$ Assembly of PL EXT 129 I $^{3,00E+03}$ $^{1,10E+05}$ Assembly of PL EXT 129 I $^{3,00E+04}$ $^{1,08E+04}$ Melting ING 137 Cs $^{3,00E+02}$ $^{2,10E+03}$ Cutting and Manipulation EXT 151 Sm $^{3,00E+02}$ $^{1,20E+03}$ Cutting and Manipulation EXT 152 Eu $^{3,00E+02}$ $^{1,20E+03}$ Cutting and Manipulation EXT 238 Pu $^{3,00E+02}$ $^{3,88E+03}$ Melting INH 239 Pu $^{3,00E+02}$ $^{9,80E+02}$ Melting INH	⁹³ Zr	3,00E+05	6,00E+04	Melting	INH
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		3,00E+02	7,70E+02	U	EXT
		3,00E+05	9,80E+07	Inhabitant	ING
^{137}Cs $^{3,00E+04}$ $^{1,00E+04}$ $^{100E+04}$ <t< td=""><td></td><td>3,00E+03</td><td>1,10E+05</td><td>Assembly of PL</td><td>EXT</td></t<>		3,00E+03	1,10E+05	Assembly of PL	EXT
151 Cs $^{3,00E+02}$ $^{2,10E+03}$ Manipulation EXT 151 Sm $^{3,00E+05}$ $^{1,08E+07}$ Melting INH 152 Eu $^{3,00E+02}$ $^{1,20E+03}$ Cutting and Manipulation EXT 238 Pu $^{3,00E+02}$ $^{3,88E+03}$ Melting INH 239 Pu $^{3,00E+02}$ $^{9,80E+02}$ Melting INH	^{129}I	3,00E+04	1,08E+04	Melting	ING
¹⁵² Eu 3,00E+02 1,20E+03 Cutting and Manipulation EXT ²³⁸ Pu 3,00E+02 3,88E+03 Melting INH ²³⁹ Pu 3,00E+02 9,80E+02 Melting INH		3,00E+02	2,10E+03	0	EXT
²³⁸ Pu 3,00E+02 1,20E+03 Manipulation ²³⁸ Pu 3,00E+02 3,88E+03 Melting INH ²³⁹ Pu 3,00E+02 9,80E+02 Melting INH	¹⁵¹ Sm	3,00E+05	1,08E+07	Melting	INH
²³⁹ Pu 3.00E+02 9.80E+02 Melting INH		3,00E+02	1,20E+03	U	EXT
²³⁹ Pu 3,00E+02 9,80E+02 Melting INH ²⁴¹ Am 3,00E+02 1,18E+03 Melting INH	²³⁸ Pu	3,00E+02	3,88E+03	Melting	INH
²⁴¹ Am 3,00E+02 1,18E+03 Melting INH	²³⁹ Pu	3,00E+02	9,80E+02	Melting	INH
	²⁴¹ Am	3,00E+02	1,18E+03	Melting	INH

Generally, derived clearance levels for majority of radionuclides could be at least one order of magnitude higher than values given in Slovak legislation for unconditional clearance.

2.6. Amount of recyclable radioactive steel

Calculation of recyclable amount of steel was performed using OMEGA code and comprehensive database of A1 NPP components and technological equipment. This code enables to determine various parameters related to decommissioning [8].

Since, practically all metal components arising from decommissioning of NPP contained mixture of radionuclides, following formula was used in order to meet clearance limits [3,6]:

$$\sum_{i=1}^{n} \frac{A_i}{Au_i} < 1 \tag{2}$$

Where:

- A_i Specific mass activity of ith radionuclide contained in material,
- Au_i Clearance level value of ith radionuclide contained in material.

Table 5 comprises calculated amount of different types of steel arising from decommissioning of A1 NPP that can be recycled and reused in motorway tunnel construction analyzed in paper. Results obtained from performed analysis indicates that concept of conditional clearance could significantly increase amount of recyclable steel and save disposal capacity. However it would be appropriate to conduct further analyses in order to decrease undue level of conservatism and to optimize the process of reuse of VLL radioactive steel.

Table 5. Calculated amount of recyclable steel (RS) arising from decommissioning of A1 NPP

Type of Steel	Amount of RS 10 µSv/year DC (kg)	Amount of RS 50 µSv/year DC (kg)
Carbon steel	112 622.96	1 045 307.57
Stainless steel	2 166.60	2 166.60
Total	114 789.56	1 047 474.17

3. Conclusion

To conclude, assessment results indicates that implementation of the concept of conditional clearance may lead to saving of considerable financial resources, which would be otherwise used for treatment, conditioning and disposal of very low level radioactive steel. Furthermore it could save valuable materials itself (particularly metals), which can be recycled and reused safely in motorway tunnel constructions.

Anyway, prior to real application of this alternative approach, it will be essential to discuss mentioned issue with all relevant stakeholders (e.g. industry, government, members of the public) and to define legal framework.

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